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TESTS OF CREOSOTED TIMBER.

By W. B. *Gregory*, M. *Am*. *Soc*. C. E.

During the last few years a quantity of literature has appeared in which the treatment of timber by preservatives has been discussed. The properties of timber, both treated and untreated, have been determined by the Forest Service, United States Department of Agriculture, and through its researches valuable knowledge has come to engineers who have to deal with the design of wooden structures. There is very little information, however, regarding the effect of time on creosoted timber, and for this reason the results given herewith may prove of interest.

The material tested consisted of southern pine stringers having a cross-section approximately 6 by 16 in. and a length of 30 ft. For the purpose of testing, each beam was cut into two parts, each about 15 ft. long. This material had been in use in a trestle of a railroad near New Orleans for 26 years. The stringers were chosen at random to determine the general condition of the trestle. The timber had been exposed to the weather and subjected to heavy train service from the time it was treated until it was tested. The annual rainfall at New Orleans is about 60 in., and the humidity of the air is high. In spite of these conditions, there was no appearance of decay on any of the specimens tested. The specifications under which the timber was treated were as follows:

TIMBER.

The timber for creosoting shall be long-leafed or southern pine. Sap surfaces on two or more sides are preferred.

Piles.—The piles shall be of long-leafed or southern pine, not less than 14 in. at the butt. They shall be free from defects impairing their strength, and shall be reasonably straight.

The piles shall be cleanly peeled, no inner skin being left on them. The oil used shall be so-called creosote oil, from London, England, and shall be of a heavy quality.

The treatment will vary according to the dimensions of the timbers and length of time they have been cut. Timbers of large and small dimensions shall not be treated in the same charge, neither shall timbers of differing stages of air seasoning, or the close-grained, be treated in the same charge with coarse or open-grained timbers.

The timbers shall be subjected first to live steam superheated to from 250 to 275 deg. Fahr., and under a 30 to 40-lb. pressure. The live steam shall be admitted into the cylinders through perforated steam pipes, and the temperature shall be obtained by using superheated steam in closed pipes in the cylinders.

The length of time this steaming shall last will depend on the size of the timbers and the length of time they have been cut. In piles and large timbers freshly cut, as long a time as 12 hours may be required. After the steaming is accomplished, the live steam shall be shut off and the superheated steam shall be maintained at a temperature of 160 deg. or more and a vacuum of from 20 to 25 in. shall be held for 4 hours or longer, if the discharge from the pumps indicates the necessity.

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Oil Treatment.—The temperature being maintained at 160 deg. Fahr., the cylinders shall be promptly filled with creosote oil at a temperature as high as practicable (about 100 deg. Fahr.). The oil shall be maintained at a pressure ranging from 100 to 120 lb., as experience and measurements must determine the length of time the oil treatment shall continue, so that the required amount of oil may be injected.

After the required amount of oil is injected, the superheated steam shall be shut off, the oil let out, the cylinders promptly opened at each end, and the timber immediately removed from the cylinder.

In the erection of timbers the sap side must be turned up, and framing or cutting of timbers shall not be permitted, if avoidable. All cut surfaces of timbers shall be saturated with hot asphaltum, thinned with creosote oil. The heads of piles when cut shall be promptly coated with the hot asphaltum and oil, even though the cut-off be temporary.

METHOD OF TESTING.

The tests were made on a Riehle 100,000-lb. machine in the Experimental Engineering Laboratory of Tulane University of Louisiana. The machine is provided with a cast-iron beam for cross-bending tests. The distance between supports was 12 ft. The method of support was as follows: Each end of the beam was provided with a steel roller which rested on the cast-iron beam of the testing machine, while above the roller, and, directly under the beam tested, there was a steel plate 6 by 8 in. in area and 1 in. thick. The area was sufficiently great to distribute the load and prevent the shearing of the fibers of the wood. The head of the Riehle machine is 10 in. wide. A plate, 3/8 in. thick, 6 in. wide and 18 in. long, was placed between the head of the machine and the beam tested.

[Illustration: *Fig*. 1.—DEFLECTON *curves beam* I]

[Illustration: *Fig*. 2.—DEFLECTON *curves beam* II]

TABLE 1.—SUMMARY OF RESULTS OF TRANSVERSE TESTS OF BEAMS AT TULANE UNIVERSITY, FEBRUARY 10TH TO MARCH 2D, 1909.

Columns in table:

1. Number of beam. 2. Top or butt of log. 3. Width, in inches. 4. Height, in inches. 5. I = (bh^3)/12 6. Actual at elastic limit. 7. Maximum. 8. At elastic limit. 9. Maximum. 10. At elastic limit. 11. E = (Pl^3)/(48dI) 12. Weight, in pounds per cubic foot.

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|  |  b  |  h  |  I  |    loads:    |S = (Plc)/(4I) |  d,  |
|  |     |     |     |              |           |inches.|
|  |------+-------+-------+-----------------+--------------
-+-------+
1  | 2 |  3  |  4  |  5  |  6  |  7  |  8  |  9  |  10  |
------+---+------+-------+-------+--------+--------+-------+
-------+-------+
I   | B | 6.28 | 15.94 | 2,120 | 22,000 | 45,900 | 2,975 | 6,200 | 0.41  |
I   | T | 6.00 | 15.69 | 1,934 | 20,000 | 38,000 | 2,915 | 5,540 | 0.465 |
|  |     |     |     |       |       |       |       |       |
II[A]| T | 6.37 | 15.81 | 2,098 | 20,000 | 43,450 | 2,722 | 5,918 | 0.380 |
II  | B | 6.41 | 16.41 | 2,360 | 16,000 | 25,040 | 1,999 | 3,130 | 0.430 |
|  |     |     |     |       |       |       |       |       |
III  | T | 5.88 | 15.68 | 1,871 | 24,000 | 45,130 | 3,608 | 6,785 | 0.535 |
III  | B | 5.88 | 15.90 | 1,965 | 21,000 | 35,190 | 3,054 | 5,120 | 0.515 |
|  |     |     |     |       |       |       |       |       |
IV  | T | 6.00 | 15.43 | 1,835 | 22,000 | 38,425 | 3,320 | 5,810 | 0.465 |
IV  | B | 6.12 | 15.87 | 2,032 | 22,000 | 35,500 | 3,090 | 4,983 | 0.660 |
|  |     |     |     |       |       |       |       |       |
V   | B | 6.00 | 16.00 | 2,048 | 22,000 | 47,000 | 3,090 | 6,610 | 0.400 |
V[A]| T | 6.00 | 15.87 | 1,999 | 14,000 | 22,050 | 1,998 | 3,145 | 0.315 |
|  |     |     |     |       |       |       |       |       |
VI[A]| B | 5.50 | 15.75 | 1,790 | 22,000 | 51,330 | 3,484 | 8,925 | 0.450 |
VI[A]| T | 5.87 | 15.62 | 1,865 | 20,000 | 44,000 | 3,013 | 6,627 | 0.410 |
|  |     |     |     |       |       |       |       |       |
VII  | B | 6.56 | 15.62 | 2,083 | 34,000 | 51,900 | 4,580 | 6,985 | 0.620 |
VII[A]| T | 6.22 | 15.62 | 1,975 | 20,000 | 49,000 | 2,845 | 6,970 | 0.380 |
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[Footnote A: Failed in longitudinal shear.]

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E    |     |
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11    |  12  |  Remarks.
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1,575,000	50.2	} Close-grained pine,
1,383,000	47.5	} long-leaf.
1,562,000	40.5	} Coarse loblolly,
979,000	42.2	} large knots.
1,489,000	40.4	} Close-grained, long-leaf
1,288,000	44.2	} no knots.
1,601,000	40.8	} Loblolly, with
1,017,000	41.5	} knots.
1,670,000	47.2	} Long-leaf yellow
1,382,000	42.1	} pine.
1,695,000	50.2	} Long-leaf yellow
1,625,000	45.2	} pine.
1,637,000	43.7	} Long-leaf yellow
1,658,000	40.2	} pine.

The deflection was measured on both sides of each beam by using silk threads stretched on each side from nails driven about 2 in. above the bottom of the beam and directly over the rollers which formed the supports. From a small piece of wood, tacked to the bottom of the beam at its center and projecting at the sides, the distance to these threads was measured. These measurements were taken to the nearest hundredth of an inch. The mean of the deflections was taken as the true deflection for any load.

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[Illustration: *Fig*. 3.—DEFLECTON *curves beam* III]

[Illustration: *Fig*. 4.—DEFLECTON *curves beam* IV]

In computing the various quantities shown in Table 1, the summary of results, the load has been assumed as concentrated at the center of the beam. While it is true that the load was spread over a length of about 12 in., due to the width of the head of the machine and the plate between it and the beam tested, it is also true that there were irregularities, such as bolt-holes and, in some cases, abrasions due to wear, that could not well be taken into account. Hence, it was deemed sufficiently accurate to consider the load as concentrated. Besides the horizontal bolt-holes, shown in the photographs, there were vertical bolt-holes, at intervals in all the beams. The latter were 7/8 in. in diameter, and in every case they were sufficiently removed from the center of the length of the beam to allow the maximum moment at the reduced section to be relatively less than that at the center of the beam. For this reason, no correction was made for these holes. The broken beams often showed that rupture started at, or was influenced by, some of the holes, especially the horizontal ones.

While some of the heavy oils of a tarry consistency remained, they were only to be found in the sappy portions of the long-leaf pine and in the loblolly (Specimens II and IV). Exposure in a semi-tropical climate for 26 years had resulted in the removal of the more volatile portions of the creosote oil. The penetration of the oil into the sap wood seemed to be perfect, while in the loblolly it varied from a fraction of an inch to 1-1/2 in. In the heart wood there was very little penetration across the grain. The timber had been framed and the holes bored before treatment. The penetration of the creosote along the grain from the holes was often from 4 to 6 in.

Circular 39 of the Forest Service, U. S. Department of Agriculture, entitled "Experiments on the Strength of Treated Timber," gives the results of a great many tests of creosoted ties, principally loblolly pine, from which the following conclusions are quoted:

"(1) A high degree of steaming is injurious to wood. The degree of steaming at which pronounced harm results will depend upon the quality of the wood and its degree of seasoning, and upon the pressure (temperature) of steam and the duration of its application. For loblolly pine the limit of safety is certainly 30 pounds for 4 hours, or 20 pounds for 6 hours." [Tables 3, 6, and 7.]

"(2) The presence of zinc chlorid will not weaken wood under static loading, although the indications are that the wood becomes brittle under impact." [Tables 3 and 4.]

[Illustration: *Fig*. 5.—DEFLECTON *curves beam* V]

[Illustration: *Fig*. 6.—DEFLECTON *curves beam* VI]

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"(3) The presence of creosote will not weaken wood of itself. Since apparently it is present only in the openings of the cells, and does not get into the cell walls, its action can only be to retard the seasoning of the wood." [Tables 3, 4, 5, and 6.]
[Illustration: *Fig*. 7.—DEFLECTON
curves beam VII]

COMPARISONS.

A comparison of the results obtained with tests made on untreated timber is interesting, and to this end Tables 2 and 3, from Circular 115, Forest Service, U. S. Department of Agriculture, by W. Kendrick Hatt, Assoc. M. Am. Soc. C. E., are quoted.
The tests made by the writer were from timber raised in Louisiana and Mississippi, while the tests quoted were from timber raised farther north. The number of tests was not sufficient to settle questions of average strength or other qualities. It will be seen, however, that the treated timber 26 years old compares favorably with the new untreated timber.

[Illustration: *Plate* I, *Fig*. 1.——*Specimenin testing machine, showing methodof support*.]

[Illustration: *Plate* I, *Fig*. 2.—*Endviews of tested timbers*.]

TABLE 2.—BENDING STRENGTH OF LARGE STICKS.

Columns in table:

A: Reference number.
B: Number of tests.
C: Moisture, per cent.
D: Rings per inch.
E: Specific gravity, dry.
F: *Weight per cubic foot*,

in pounds.
G: As tested.
H: Oven dry.
I: Fiber stress at elastic limit, in pounds per square inch.
J: Modulus of rupture, in pounds per square inch.
K: Modulus of elasticity, in thousands of pounds per square inch.
L: Elastic resilience, in inch pounds per cubic inch.
M: Number failing by longitudinal shear.

Loblolly pine.

A	Locality of Growth.	*dimensions.* Section, in inches.	Span, in feet	Grade.	Condition of seasoning.		B	C	D
		6 by 7							
		6 by 10	10						
1	South	4 by 12	to	Square	Green	Average		48.0	5.7
	Carolina.	6 by 16	15.5	edge		Maximum	42	92.1	11.7
		8 by 14				Minimum		30.2	2.3

Long-leaf pine.

A	Locality of Growth.	Section, in inches	Span, in feet	Grade.	Condition of seasoning.		B	C	D
						Average		25.0	13.7
6	South	6 by 8	15	Merchant-	Partially	Maximum	22	40.3	25.4
	Carolina.	10 by 16		able	air dry	Minimum		17.3	6.2
						Average		27.3	18.0
7	Georgia.	10 by 12	15	Merchant-	Partially	Maximum	22	34.5	29.0
				able	air dry.	Minimum		20.0	11.0

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|   | Locality|    |     F     |     |      |     |    |   |            |
|   |    of   |    +---------+      |      |     |    |   |            |
| A | Growth. |  E |     |     | I   |  J   | K   | L  | M |  Remarks.  |
|   |         |    |  G |  H |     |      |     |    |   |            |
|   |         |    |    |    |     |      |     |    |   |            |
+---+---------+----+----+----+-----+------+-----+----+---+--
----------+
|   |         |    |    |    |     |      |     |    |Moisture    |
|   |         |    |    |    |     |      |     |    |above       |
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Long-leaf pine.

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+---+---------+----+----+----+-----+------+-----+----+-
--+------------+
|   |         |0.58|45.6|36.2|3,800| 7,160|1,560|0.53|   |            |
| 6 |South    |0.76|60.0|47.5|4,970|10,020|2,010|0.78| 9 |            |
|   |Carolina.|0.50|39.4|31.2|2,220| 5,450|1,190|0.21|   |            |
+---+---------+----+----+----+-----+------+-----+----+---+--
----------+
|   |         |0.69|54.7|42.9|5,581| 8,384|1,820| -- |   |Excellent   |
| 7 |Georgia. |0.79| -- |49.4|9,600|11,410|2,920| -- | 6 |merchantable|
|   |         |0.50| -- |31.4|3,547| 4,836|1,167| -- |   |grade.      |
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TABLE 3.—LOBLOLLY PINE.—BENDING TESTS ON BEAMS SEASONED UNDER
DIFFERENT CONDITIONS.
(8 by 16-in. section; 13-1/2 to 15-ft. span.)

Columns in table:

A. Number of tests.
B. Fiber stress at elastic limit, in pounds per square inch.
C. Modulus of rupture, in pounds per square inch.
D. Longitudinal shear at maximum load, in pounds per square inch.
E. Modulus of elasticity, in thousands of pounds per square inch.
F. Percentage of moisture.
G. Rings per inch.
H. Weight per cubic foot, oven dry, in pounds.
I. Condition of seasoning.

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	A	B	C	D	E	F	G	H	I
Average		3,580	5,480	364_{4}	1,780	23.2	9.4	33.7	Air dry,
Maximum	4	4,070	6,600	440	1,987	24.3	11.5	34.5	3-1/2 months
Minimum		3,090	5,000	327	1,530	21.5	8.0	32.5	in the open.
Average		4,512	5,060	338_{3}	1,685	20	7.7	33.9	Kiln dry,
Maximum	5	5,840	7,320	488	1,790	22	10.2	38.0	6 days.
Minimum		3,180	2,150	143	1,410	18	4.7	27.7	
Average		4,331	6,721	493_{9}	1,688	—	7.7	—	Air dry, 21
Maximum	12	4,990	8,560	620	2,002	—	9.5	—	months under
Minimum		3,110	5,160	380	1,398	—	5.5	—	shelter.

Note.—Figures written as subscripts to the figures for longitudinal shear indicate the number of sticks failing in that manner.

[Illustration: *Plate* II.—*Sideviews of tested timbers*.]

TABLE 4.—LOAD AND DEFLECTION LOG. BEAM I.

Columns in table:

A: Load, in pounds.
B: Reading.
C: Total deflection.
D: Mean total deflection.

Date: February 26th, 1909.
Date: February 24th, 1909. *l* = 12 ft.;
l = 12 ft.; *b*
(mean) = 6-9/32 in.; *b* (mean)
= 6 in.; *h* (mean) = 15-15/16 in.;
h (mean) = 15.69 in.; *c* = 7.97
in. *c* = 7.84 in.
Time = 1 hour.

No.	P	*deflection, in inches.*					P	*deflection, in inches.*				
	A	B	C	B	C	D	A	B	C	B	C	D
1	0	1.86	0	1.88	0	0	0	1.83	0	1.86	0	0
2	2,000	1.92	0.05	1.90	0.02	0.035	2,000	1.87	0.04	1.90	0.04	0.04
3	4,000	1.96	0.10	1.94	0.06	0.080	4,000	1.91	0.08	1.96	0.10	0.090
4	6,000	1.99	0.13	1.98	0.10	0.115	6,000	1.96	0.13	2.00	0.14	0.135
5	8,000	2.03	0.17	2.02	0.14	0.155	8,000	2.00	0.17	2.04	0.18	0.175
6	10,000	2.05	0.19	2.06	0.18	0.185	10,000	2.04	0.21	2.08	0.22	0.215
7	12,000	2.10	0.24	2.09	0.21	0.225	12,000	2.09	0.26	2.13	0.27	0.265
8	14,000	2.13	0.27	2.13	0.25	0.260	14,000	2.14	0.31	2.18	0.32	0.315
9	16,000	2.17	0.31	2.16	0.28	0.295	16,000	2.19	0.36	2.23	0.37	0.365
10	18,000	2.20	0.34	2.20	0.32	0.330	18,000	2.24	0.41	2.28	0.42	0.415

[Footnote B: First crack.]

TABLE 4.—(*Continued.*)—LOAD AND DEFLECTION LOG. BEAM II.

Columns in table:

A: Load, in pounds.
B: Reading.
C: Total deflection.
D: Mean total deflection.

Date: February 20th, 1909.
Date: — *l* = 12 ft.;
l = 12 ft.; *b* (mean)
= 6.38 in.; *b* (mean) = 6.41
in.; *h* (mean) = 15.81 in.;

h (mean) = 16.41 in.; *c* = 7.91 in.
c = 8.20 in.
Time = 47.5 min.

No.	P (A)	DEFLECTION, IN INCHES. B	C	B	C	D	P (A)	DEFLECTION, IN INCHES. B	C	B	C	D
1	0	1.65	0	1.68	0	0	0	1.86	0	1.87	0	0
2	2,000	1.69	0.04	1.72	0.04	0.040	2,000	1.91	0.05	1.92	0.05	0.05
3	4,000	1.73	0.08	1.77	0.09	0.085	4,000	1.98	0.12	1.98	0.11	0.115
4	6,000	1.76	0.11	1.80	0.12	0.115	6,000	2.05	0.19	2.02	0.15	0.170
5	8,000	1.80	0.15	1.83	0.15	0.150	8,000	2.07	0.21	2.08	0.21	0.210
6	10,000	1.83	0.18	1.86	0.18	0.180	10,000	2.13	0.27	2.13	0.26	0.265
7	12,000	1.87	0.22	1.90	0.22	0.220	12,000	2.18	0.32	2.18	0.31	0.315
8	14,000	1.91	0.26	1.94	0.26	0.260	14,000	2.25	0.39	2.24	0.37	0.380

[Footnote C: First crack.]

TABLE 4.—(*Continued.*)—LOAD AND DEFLECTION LOG. BEAM III.

Columns in table:

A: Load, in pounds.
B: Reading.
C: Total deflection.
D: Mean total deflection.

Date: February 13th, 1909.
Date: — *l* = 12 ft.;
l = 12 ft.; *b* (mean) = 5.88 in.;
b (mean) = 5.88 in.; *h* (mean) = 15.63 in.;
h (mean) = 15.9 in.; *c* = 7.82 in.
c = 7.95 in.
Time = 45 min.

No.	P	DEFLECTION, IN INCHES.					P	DEFLECTION, IN INCHES.				
	A	B	C	B	C	D	A	B	C	B	C	D
1	0	1.23	0	1.06	0	0	0	1.67	0	1.63	0	0
2	2,000	1.27	.04	1.10	0.04	0.040	2,000	1.70	0.03	1.68	0.05	0.040
3	4,000	1.32	0.09	1.13	0.07	0.080	4,000	1.72	0.05	1.72	0.09	0.070
4	6,000	1.37	0.14	1.17	0.11	0.125	6,000	1.82	0.15	1.78	0.15	0.150
5	8,000	1.42	0.19	1.22	0.16	0.175	8,000	1.86	0.19	1.82	0.19	0.190
6	10,000	1.47	0.24	1.26	0.20	0.220	10,000	1.90	0.23	1.87	0.24	0.235
7	12,000	1.51	0.28	1.31	0.25	0.265	12,000	1.97	0.30	1.92	0.29	0.295
8	14,000	1.55	0.32	1.35	0.29	0.305	14,000	2.00	0.33	1.98	0.35	0.340
9	16,000	1.60	0.37	1.40	0.34	0.355	16,000	2.03	0.36	2.04	0.41	0.385

TABLE 4.—(*Continued.*)—LOAD AND DEFLECTION LOG. BEAM IV.

Columns in table:

A: Load, in pounds.
B: Reading.
C: Total deflection.
D: Mean total deflection.

Date: February 16th, 1909.
Date: February 10th, 1909. *l* = 12 ft.;
l = 12 ft.; *b* (mean) = 6.0 in.; *b* (mean) = 6.12 in.; *h* (mean) = 15.43 in.;
h (mean) = 15.87 in.; *c* = 7.71 in.
c = 7.93 in.
Time = 30 min.

No.	P	DEFLECTION, IN INCHES.					P	DEFLECTION, IN INCHES.				
	A	B	C	B	C	D	A	B	C	B	C	D
1	0	2.28	0	2.05	0	0	0	1.44	0	1.58	0	0
2	2,000	2.31	0.03	2.10	0.05	0.040	2,000	1.50	0.06	1.64	0.06	0.06

3	4,000	2,34	0.06	2.14	0.09	0.075	4,000	1.55	0.11	1.70	0.12	0.115
4	6,000	2.40	0.12	2.19	0.14	0.130	6,000	1.62	0.18	1.76	0.18	0.180
5	8,000	2.43	0.15	2.23	0.18	0.165	8,000	1.68	0.24	1.82	0.24	0.240
6	10,000	2.47	0.19	2.28	0.23	0.210	10,000	1.72	0.28	1.89	0.31	0.295
7	12,000	2.51	0.23	2.32	0.27	0.250	12,000	1.80	0.36	1.94	0.36	0.360

TABLE 4.—(*Continued.*)—LOAD
AND DEFLECTION LOG. BEAM V.

Columns in table:

A: Load, in pounds.
B: Reading.
C: Total deflection.
D: Mean total deflection.

Date: —
Date: February 27th, 1909. *l* = 12 ft.; *l* = 12 ft.;
b (mean) = 6 in.; *b* (mean) = 6 in.; *h* (mean) = 16 in.;
h (mean) = 15.87 in.; *c* = 8 in. *c* = 7.94 in. Time = 40 min.

No.	P	DEFLECTION, IN INCHES.					P	DEFLECTION, IN INCHES.				
	A	B	C	B	C	D	A	B	C	B	C	D
1	0	1.97	0	1.37	0	0	0	1.31	0	1.25	0	0
2	2,000	2.01	0.04	1.40	0.03	0.035	2,000	1.37	0.06	1.31	0.06	0.06
3	4,000	2.06	0.09	1.43	0.06	0.075	4,000	1.41	0.10	0.36	0.11	0.105
4	6,000	2.08	0.11	1.47	0.10	0.105	6,000	1.46	0.15	0.40	0.15	0.150
5	8,000	2.11	0.14	1.50	0.13	0.135	8,000	1.49	0.18	0.45	0.20	0.190
6	10,000	2.16	0.19	1.54	0.17	0.180	10,000	1.54	0.23	1.49	0.24	0.235
7	12,000	2.19	0.22	1.57	0.20	0.210	12,000	1.58	0.27	1.53	0.28	0.275

TABLE 4.—(*Continued.*)—LOAD
AND DEFLECTION LOG. BEAM VI.

Columns in table:

A: Load, in pounds.

B: Reading.
C: Total deflection.
D: Mean total deflection.

Date: February 12th, 1909.
Date: February 13th, 1909. *l* = 12 ft.;
l = 12 ft.; *b*
(mean) = 5.5 in.; *b* (mean)
= 5.87 in.; *h* (mean) = 15.75 in.;
h (mean) = 15.62 in.; *c* = 7.88
in. *c* = 7.81 in.
Time = 40 min.

No.	P A	DEFLECTION, IN INCHES. B	C	B	C	D	P A	DEFLECTION, IN INCHES. B	C	B	C	D
1	0	1.22	0	1.30	0	0	0	1.28	0	1.30	0	0
2	2,000	1.26	0.04	1.34	0.04	0.04	2,000	1.30	0.02	1.35	0.05	0.035
3	4,000	1.29	0.07	1.38	0.08	0.075	4,000	1.36	0.08	1.39	0.09	0.085
4	6,000	1.33	0.11	1.42	0.12	0.115	6,000	1.40	0.12	1.44	0.14	0.130
5	8,000	1.37	0.15	1.47	0.17	0.160	8,000	1.43	0.15	1.47	0.17	0.160
6	10,000	1.42	0.20	1.51	0.21	0.205	10,000	1.47	0.19	1.51	0.21	0.200
7	12,000	1.45	0.23	1.55	0.25	0.240	12,000	1.51	0.23	1.56	0.26	0.245
8	14,000	1.50	0.28	1.59	0.29	0.285	14,000	1.55	0.27	1.60	0.30	0.285
9	16,000	1.54	0.32	1.63	0.33	0.325	16,000	1.59	0.31	1.64	0.34	0.325

TABLE 4.—(*Continued.*)—LOAD AND DEFLECTION LOG. BEAM VII.

Columns in table:

A: Load, in pounds.
B: Reading.
C: Total deflection.
D: Mean total deflection.

Date: March 2d, 1909. Date: February 20th, 1909.
l = 12 ft.; *l* = 12 ft.;
b (mean) = 6.56 in.; *b* (mean) = 6.22 in.;
h (mean) = 15.62 in.; *h* (mean) = 15.62 in.;
c = 7.81 in. *c* = 7.81 in.

Time = 1 hr. Time = 33 min.

No.	P	DEFLECTION, IN INCHES.					P	DEFLECTION, IN INCHES.				
	A	B	C	B	C	D	A	B	C	B	C	D
1	0	1.84	0	1.71	0	0	0	1.69	0	1.73	0	0
2	2,000	1.88	0.04	1.74	0.03	0.035	2,000	1.72	0.03	1.77	0.04	0.035
3	4,000	1.92	0.08	1.79	0.08	0.080	4,000	1.76	0.07	1.80	0.07	0.070
4	6,000	1.96	0.12	1.81	0.10	0.110	6,000	1.80	0.11	1.84	0.11	0.110

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5 | 8,000|2.00|0.16|1.85|0.14|0.150|| 8,000 |1.84|0.15|1.87|0.14|0.145
6 |10,000|2.03|0.19|1.89|0.18|0.185||10,000 |1.88|0.19|1.92|0.19|0.190
7 |12,000|2.06|0.22|1.93|0.22|0.220||12,000 |1.91|0.22|1.95|0.22|0.220
8 |14,000|2.11|0.27|1.95|0.24|0.255||14,000 |1.95|0.26|2.00|0.27|0.265
9 |16,000|2.14|0.30|1.99|0.28|0.290||16,000 |1.99|0.30|2.03|0.30|0.300
10 |18,000|2.18|0.34|2.03|0.32|0.330||18,000 |2.03|0.34|2.06|0.33|0.335
11 |20,000|2.22|0.38|2.05|0.34|0.360||20,000 |2.07|0.38|2.11|0.38|0.380
12 |22,000|2.25|0.41|2.10|0.39|0.400||22,000 |2.11|0.42|2.16|0.43|0.425
13 |24,000|2.29|0.45|2.13|0.42|0.435||24,000 |2.15|0.46|2.20|0.47|0.465
14 |26,000|2.32|0.48|2.17|0.46|0.470||26,000 |2.19|0.50|2.24|0.51|0.505
15 |28,000|2.36|0.52|2.21|0.50|0.510||28,000 |2.23|0.54|2.28|0.55|0.545
16 |30,000|2.40|0.56|2.25|0.54|0.550||30,000 |2.27|0.58|2.33|0.60|0.590
17 |32,000|2.43|0.59|2.29|0.58|0.585||32,000 |2.32|0.63|2.37|0.64|0.635
18 |34,000|2.47|0.63|2.32|0.61|0.620||34,000 |2.36|0.67|2.42|0.69|0.680
19 |36,000|2.51|0.67|2.37|0.66|0.665||36,000 |
20 |38,000|2.56|0.72|2.41|0.70|0.710||
||
27,000 lb., First Crack; ||28,000 lb., First Crack;
51,900 lb., Failed. ||49,000 lb., Failed.
||
At Elastic Limit: Load, 34,000 lb.; ||At Elastic Limit: Load, 20,000 lb.;
deflection, 0.62 in.; || deflection, 0.38 in.;
S, 4,580 lb. || S, 2,845 lb.
||
Maximum: Load, 51,900 lb.; ||Maximum: Load, 49,000 lb.;
deflection,.....; || deflection,.....;
S, 6,985 lb. || S, 6,970 lb.
||
E = 1,637,000 lb. || E = 1,658,000 lb.
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10 |18,000|1.58|0.36|1.68|0.38|0.370||18,000  |1.62|0.34|1.69|0.39|0.365
11 |20,000|1.61|0.39|1.72|0.42|0.405||20,000  |1.66|0.38|1.74|0.44|0.410
12 |22,000|1.66|0.44|1.76|0.46|0.450||22,000  |1.71|0.43|1.80|0.50|0.465
13 |24,000|1.81|0.59|1.81|0.51|0.550||24,000  |1.77|0.49|1.84|0.54|0.515
14 |26,000|1.86|0.64|1.86|0.56|0.600||26,000  |1.83|0.55|1.90|0.60|0.575
15 |28,000|1.91|0.69|1.91|0.61|0.650||28,000  |1.90|0.62|1.97|0.67|0.645
16 |30,000|1.96|0.74|1.96|0.66|0.700||30,000  |1.97|0.69|2.02|0.72|0.705
17 |32,000|2.00|0.78|2.02|0.72|0.750||32,000  |2.12|0.84|2.10|0.80|0.820
18 |34,000|2.04|0.82|2.11|0.81|0.815||34,000  |2.20|0.92|2.16|0.86|0.885
19 |36,000|2.10|0.88|2.20|0.90|0.890||36,000  |2.29|1.01|2.24|0.94|0.975
20 |38,000|2.16|0.94|2.25|0.95|0.945||38,000  |2.39|1.11|2.32|1.02|1.065
21 |40,000|2.28|1.06|2.38|1.08|1.070||
22 |42,000|2.38|1.16|2.42|1.12|1.140||
23 |44,000|2.44|1.22|2.52|1.22|1.220||
24 |46,000|2.53|1.31|2.60|1.30|1.305||
25 |48,000|2.66|1.44|2.71|1.41|1.425||
26 |50,000|2.78|1.56|2.87|1.57|1.565||
||
33,000 lb., First Crack;          ||24,000 lb., First Crack;
51,330 lb., Failed.               ||44,000 lb., Failed.
||
At Elastic Limit:  Load, 22,000 lb.; ||At Elastic Limit:  Load, 20,000 lb.;
deflection, 0.45 in.;             ||  deflection, 0.41 in.;
S, 3,484 lb.                      ||  S, 3,018 lb.
||
Maximum:  Load, 51,330 lb.;       ||Maximum:  Load, 44,000 lb.;
deflection,.....;                 ||  deflection,.....;
S, 8,925 lb.                      ||  S, 6,627 lb.
||
E =  1,695,000 lb.                ||  E =  1,625,000 lb.
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8 |14,000|2.22|0.25|1.61|0.24|0.245||14,000 |1.62|0.31|1.57|0.32|0.315
9 |16,000|2.25|0.28|1.65|0.28|0.280||16,000 |1.68|0.37|1.65|0.40|0.385
10 |18,000|2.29|0.32|1,69|0.32|0.320||18,000 |1.78|0.41|1.71|0.46|0.435
11 |20,000|2.32|0.35|1.73|0.36|0.355||20,000 |1.99|0.68|1.97|0.72|0.700
12 |22,000|2.36|0.39|1.78|0.41|0.400||
13 |24,000|2.39|0.42|1.83|0.46|0.440||
14 |26,000|2.42|0.45|1.85|0.48|0.465||
15 |28,000|2.47|0.50|1.90|0.53|0.515||
16 |30,000|2.50|0.53|1.95|0.58|0.565||
17 |32,000|2.54|0.57|1.99|0.62|0.595||
18 |34,000|2.59|0.62|2.04|0.67|0.645||
19 |36,000|2.63|0.66|2.09|0.72|0.690||
20 |38,000|2.68|0.71|2.17|0.80|0.755||
21 |40,000|2.73|0.76|2.21|0.84|0.800||
22 |42,000|2.80|0.83|2.30|0.93|0.880||
23 |44,000|2.90|0.93|2.40|1.03|0.980||
||
25,000 lb. Slight Crack; ||20,000 lb. First Crack;
47,000 lb. Failed. ||22,050 lb. Failed.
||
At Elastic Limit: Load, 22,000 lb.; ||At Elastic Limit: Load, 14,000 lb.;
deflection, 0.40 in.; || deflection, 0.315 in.;
S, 3,090 lb. || *S*, 1,998 lb.
||
Maximum: Load, 47,000 lb.; ||Maximum: Load, 22,050 lb.;
deflection,.......; || deflection,.......;
S, 6,610 lb. || *S*, 3,145 lb.
||
E = 1,670,000 lb. || *E* = 1,382,000 lb.
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8 |14,000|2.54|0.26|2.37|0.32|0.290||14,000 |1.85|0.41|2.00|0.42|0.415
9 |16,000|2.59|0.31|2.41|0.36|0.335||16,000 |1.90|0.46|2.06|0.48|0.470
10 |18,000|2.62|0.34|2.45|0.40|0.370||18,000 |1.98|0.54|2.13|0.55|0.545
11 |20,000|2.68|0.40|2.50|0.45|0.425||20,000 |2.03|0.59|2.19|0.61|0.600
12 |22,000|2.72|0.44|2.54|0.49|0.465||22,000 |2.09|0.65|2.25|0.67|0.660
13 |24,000|2.78|0.50|2.60|0.55|0.525||24,000 |2.15|0.71|2.33|0.75|0.730
14 |26,000|2.82|0.54|2.65|0.60|0.570||26,000 |2.23|0.79|2.42|0.84|0.815
15 |28,000|2.87|0.59|2.69|0.64|0.615||28,000 |2.32|0.88|2.49|0.91|0.895
16 |30,000|2.91|0.63|2.74|0.69|0.660||30,000 |2.42|0.98|2.62|1.04|1.010
17 |32,000|2.97|0.69|2.78|0.73|0.710||32,000 |2.56|1.12|2.74|1.16|1.140
18 |34,000|3.01|0.73|2.85|0.80|0.765||34,000 |2.67|1.23|2.87|1.29|1.265
19 |36,000|3.07|0.79|2.90|0.85|0.820||
20 |38,000|3.14|0.86|2.98|0.93|0.895||
||
34,000 lb. First Crack; ||28,360 lb. Cracked;
38,425 lb. Failed. ||35,500 lb, Failed.
||
At Elastic Limit: Load, 22,000 lb.; ||At Elastic Limit: Load, 22,000 lb.;
deflection, 0.465 in.; || deflection, 0.66 in.;
S 3,320 lb. || S, 3,090 lb.
||
Maximum: Load, 38,425 lb.; ||Maximum: Load, 35,500 lb.;
deflection,.....; || deflection,.....;
S 5,810 lb. || S 4,983 lb.
||
E = 1,601,000 lb. || E = 1,017,000 lb.
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10 |18,000|1.64|0.41|1.44|0.38|0.395||18,000  |2.10|0.43|2.09|0.46|0.445
11 |20,000|1.68|0.45|1.49|0.43|0.440||20,000  |2.13|0.46|2.14|0.51|0.485
12 |22,000|1.72|0.49|1.54|0.48|0.485||22,000  |2.20|0.53|2.20|0.57|0.550
13 |24,000|1.78|0.55|1.58|0.52|0.535||24,000  |2.26|0.59|2.26|0.63|0.610
14 |26,000|1.82|0.59|1.64|0.58|0.585||26,000  |2.31|0.64|2.32|0.69|0.665
15 |28,000|1.88|0.65|1.68|0.62|0.635||28,000  |2.38|0.71|2.40|0.77|0.740
16 |30,000|1.92|0.69|1.73|0.67|0.680||30,000  |2.42|0.75|2.47|0.84|0.795
17 |32,000|1.97|0.74|1.79|0.73|0.735||32,000  |2.49|0.82|2.55|0.92|0.870
18 |34,000|2.02|0.79|1.85|0.79|0.790||34,000  |2.58|0.91|2.62|0.99|0.950
19 |36,000|2.07|0.84|1.90|0.84|0.840||
20 |38,000|2.13|0.90|1.97|0.91|0.915||
21 |40,000|2.20|0.97|2.03|0.97|0.970||
22 |42,000|2.27|1.04|2.11|1.05|1.045||
23 |44,000|2.37|1.14|2.21|1.15|1.145||
||
39,100 lb.  First Crack;           ||22,000 lb.  First Crack;
45,130 lb.  Failed.                ||35,190 lb.  Failed.
||
At Elastic Limit:  Load, 24,000 lb.; ||At Elastic Limit:  Load, 21,000 lb.;
deflection, 0.535 in.;          ||  deflection, 0.515 in.;
S 3,608 lb.                     ||  S, 3,054 lb.
||
Maximum:  Load, 45,130 lb.;        ||Maximum:  Load, 35,190 lb.;
deflection,.....;               ||  deflection,.....;
S 6,785 lb.                     ||  S 5,120 lb.
||
E = 1,489,000 lb.               ||  E = 1,288,000 lb.
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9 |16,000|1.95|0.30|1.98|0.30|0.300||16,000 |2.30|0.44|2.29|0.42|0.430
10 |18,000|1.98|0.33|2.02|0.34|0.335||18,000[C]|2.35|0.49|2.
35|0.48|0.485
11 |20,000|2.03|0.38|2.06|0.38|0.380||20,000 |2.44|0.58|2.42|0.55|0.565
12 |22,000|2.07|0.42|2.10|0.42|0.420||22,000 |2.54|0.68|2.54|0.67|0.675
13 |24,000|2.11|0.46|2.14|0.46|0.460||25,040 | Failed
14 |26,000|2.15|0.50|2.18|0.50|0.500||
15 |28,000|2.18|0.53|2.22|0.54|0.535||
16 |30,000|2.23|0.58|2.26|0.58|0.580||
17 |32,000|2.27|0.62|2.30|0.62|0.620||
18 |34,000|2.32|0.67|2.35|0.67|0.670||
19 |36,000|2.37|0.72|2.40|0.72|0.720||
20 |38,000|2.42|0.77|2.45|0.77|0.770||
21 |40,000|2.48|0.83|2.50|0.82|0.825||
22 |42,000|2.53|0.88|2.56|0.88|0.880||
23 |43,450| Fracture. ||
24 |45,710| Failed. ||
||
At Elastic Limit: Load, 20,000 lb.; ||At Elastic Limit: Load, 16,000 lb.;
deflection, 0.38 in.; || deflection, 0.43 in.;
S, 2,722 lb. || S, 1,999 lb.
||
Maximum: Load, 43,450 lb.; ||Maximum: Load, 25,040 lb.;
deflection,.....; || deflection,.....;
S, 5,918 lb. || S, 3,130 lb.
||
E = 1,562,000 lb. || E = 979,000 lb.
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11 |20,000|2.24|0.36|2.25|0.37|0.365||20,000 |2.29|0.46|2.33|0.47|0.465
12 |22,000|2.28|0.42|2.28|0.40|0.410||22,000 |2.34|0.51|2.39|0.53|0.520
13 |24,000|2.32|0.46|2.32|0.44|0.450||24,000 |2.39|0.56|2.43|0.57|0.565
14 |26,000|2.36|0.50|2.36|0.48|0.490||26,000 |2.44|0.61|2.48|0.62|0.615
15 |28,000|2.40|0.54|2.39|0.51|0.525||28,000 |2.49|0.66|2.53|0.67|0.685
16 |30,000|2.43|0.57|2.44|0.56|0.565||30,000 |2.55|0.72|2.58|0.72|0.720
17 |32,000|2.48|0.62|2.48|0.60|0.610||32,000 |2.61|0.78|2.65|0.79|0.785
18 |34,000|2.52|0.68|2.53|0.65|0.655||34,000[B]|2.68|0.85|2.
70|0.84|0.845
19 |36,000|2.56|0.70|2.56|0.68|0.690||36,000 |2.74|0.91|2.78|0.92|0.915
20 |38,000|2.61|0.75|2.62|0.74|0.745||38,000 | Broke.
21 |40,000|2.65|0.79|2.67|0.79|0.790||
22 |42,000|2.70|0.84|2.73|0.85|0.845||
23 |44,000|2.75|0.89|2.77|0.89|0.890||
||
37,500 lb., First Crack; ||
45,900 lb., Failed. ||
||
At Elastic Limit: Load, 22,000 lb.; ||At Elastic Limit: Load, 20,000 lb.;
deflection, 0.41 in.; || deflection, 0.465 in.;
S, 2,975 lb. || *S*, 2,975 lb.
||
Maximum: Load, 45,900 lb.; ||Maximum: Load, 38,000 lb.;
deflection,.....; || deflection,.....;
S, 6,209 lb. || *S*, 5,540 lb.
||
E = 1,575,000 lb. || *E* = 1,383,000 lb.
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1	South	0.50	46.2	31.2	3,150	5,580	1,426	0.45		saturation
	Carolina.	0.60	56.8	37.5	5,210	8,460	1,920	0.99	7	point in
		0.40	35.6	25.0	1,675	3,120	905	0.07		all cases.
2	South	0.50	40.0	31.2	3,380	5,650	1,435	0.45		Moisture
	Carolina.	0.55	43.7	34.4	4,610	8,090	1,880	0.76	0	from 25 to
		0.45	35.6	28.1	2,115	3,600	1,152	0.20		30 per cent.
	South	0.50	37.5	31.2	2,970	5,690	1,340	0.39		Moisture
3	Carolina.	0.58	45.6	36.2	4,850	8,100	2,040	0.69	2	less than
		0.41	31.2	25.6	1,730	2,910	906	0.10		25 per cent.
		0.46	35.6	28.8	3,260	5,180	1,180	0.51		
4	Virginia.	0.58	43.1	36.2	5,300	8,950	1,728	1.05	0	
		0.37	30.0	23.1	1,280	2,180	606	0.13		
		0.43	43.7	26.9	1,935	3,490	744	0.31		Very rapid
5	Virginia.	0.51	51.9	31.9	3,185	4,720	1,193	0.78	0	growth; poor
		0.35	35.0	21.9	956	2,180	357	0.12		quality.

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|   |         | 8 by 16|     |         |          |       |   |     |    |
+---+---------+--------+-----+---------+----------+-------+-
--+-----+----+
|   |         | 6 by  7|     |         |          |       |   |     |    |
|   |         | 4 by 12|  10 |         |          |       |   |     |    |
| 2 |South    | 6 by 10|  to |  Square |Partially |Average|   | 27.7| 5.0|
|   |Carolina.| 6 by 16|  16 |  edge   |air dry.  |Maximum| 18| 29.2| 8.2|
|   |         | 8 by 16|     |         |          |Minimum|   | 25.5| 2.5|
|   |         |10 by 16|     |         |          |       |   |     |    |
+---+---------+--------+-----+---------+----------+-------+-
--+-----+----+
|   |         | 6 by  7|  10 |         |          |       |   |     |    |
|   |South    | 4 by 12|  to |  Square |Partially |Average|   | 21.0| 5.6|
| 3 |Carolina.| 6 by 10|  15 |  edge   |air dry.  |Maximum| 19| 24.9|17.2|
|   |         | 6 by 16|     |         |          |Minimum|   | 15.0| 2.7|
+---+---------+--------+-----+---------+----------+-------+-
--+-----+----+
|   |         |        |  6  |         |          |Average|   | 22.4| 4.8|
| 4 |Virginia.| 8 by  8| to  |  Square |Partially |Maximum| 12| 27.7| 8.8|
|   |         |        | 16  |  edge   |air dry.  |Minimum|   | 17.8| 2.5|
+---+---------+--------+-----+---------+----------+-------+-
--+-----+----+
|   |         |        | 6   |         |          |Average|   | 64.0| 3.0|
| 5 |Virginia.| 8 by  8| to  |  Square | Green    |Maximum| 17|100.5| 4.0|
|   |         |        |15.5 |  edge   |          |Minimum|   | 38.8| 2.5|
+---+---------+--------+-----+---------+----------+-------+-
--+-----+----+
```